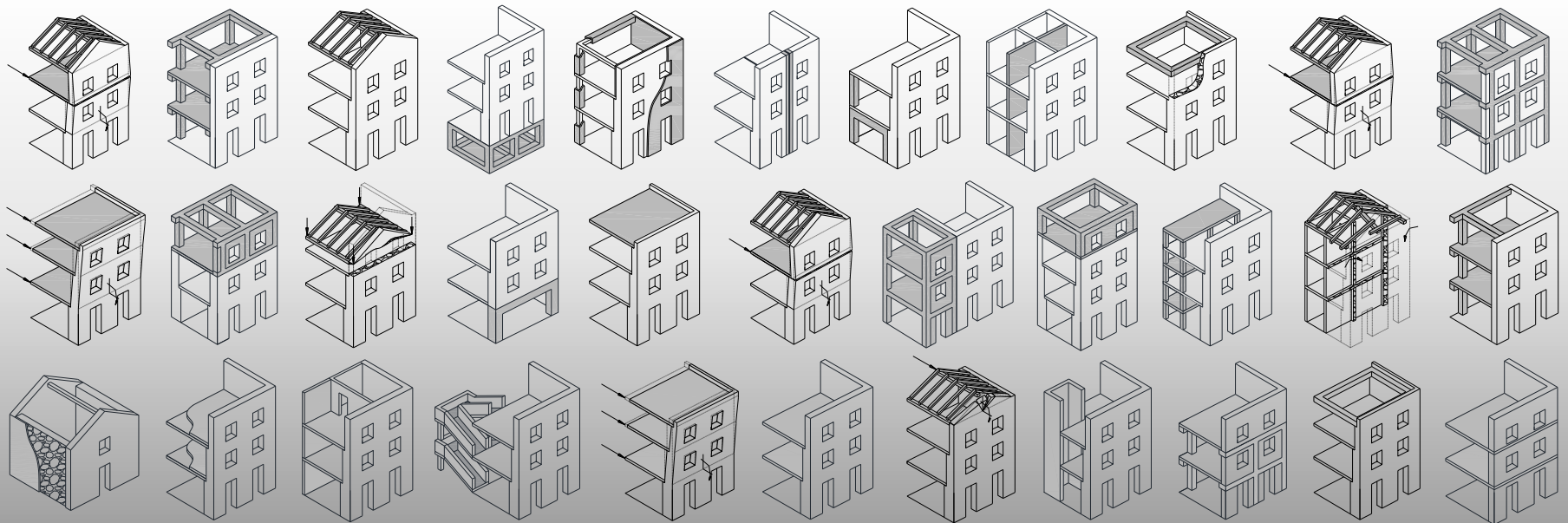


A BIM-BASED METHODOLOGY FOR THE SEISMIC PERFORMANCE ASSESSMENT OF EXISTING URM-RC BUILDINGS

Gonçalo Correia Lopes (3rd year, U. Aveiro)

Supervision: Romeu Vicente (U. Aveiro), Miguel Azenha (U. Minho), Tiago Miguel Ferreira (U. Minho)



Presentation summary

- **Planned tasks and research methodology**

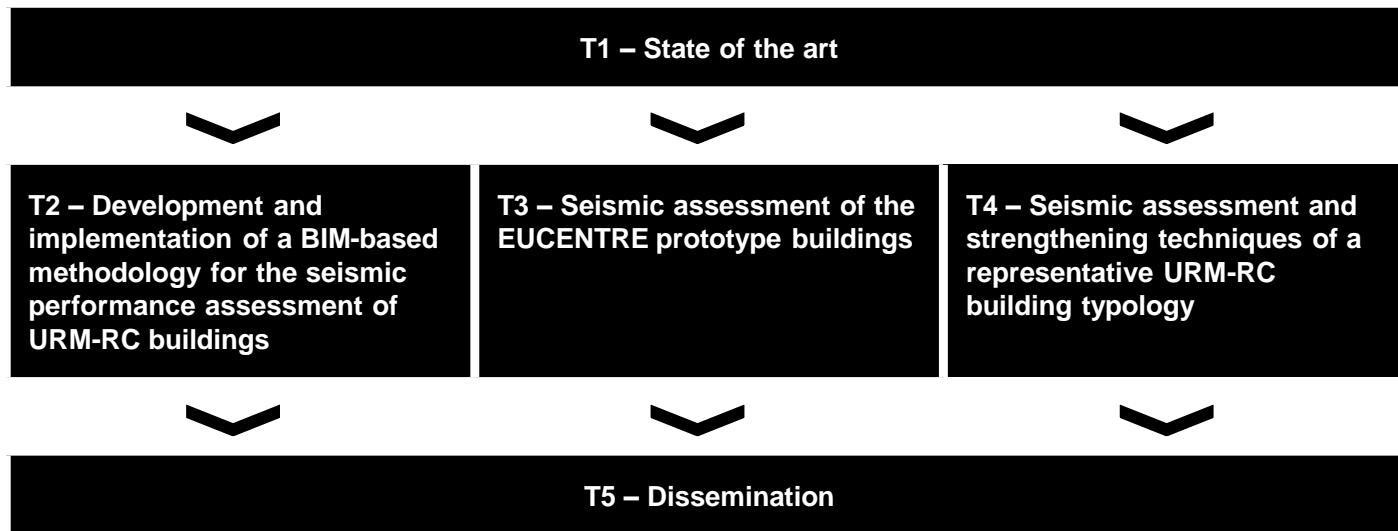
 **Work done** — Carried out research work

 **Work in progress** — Ongoing tasks

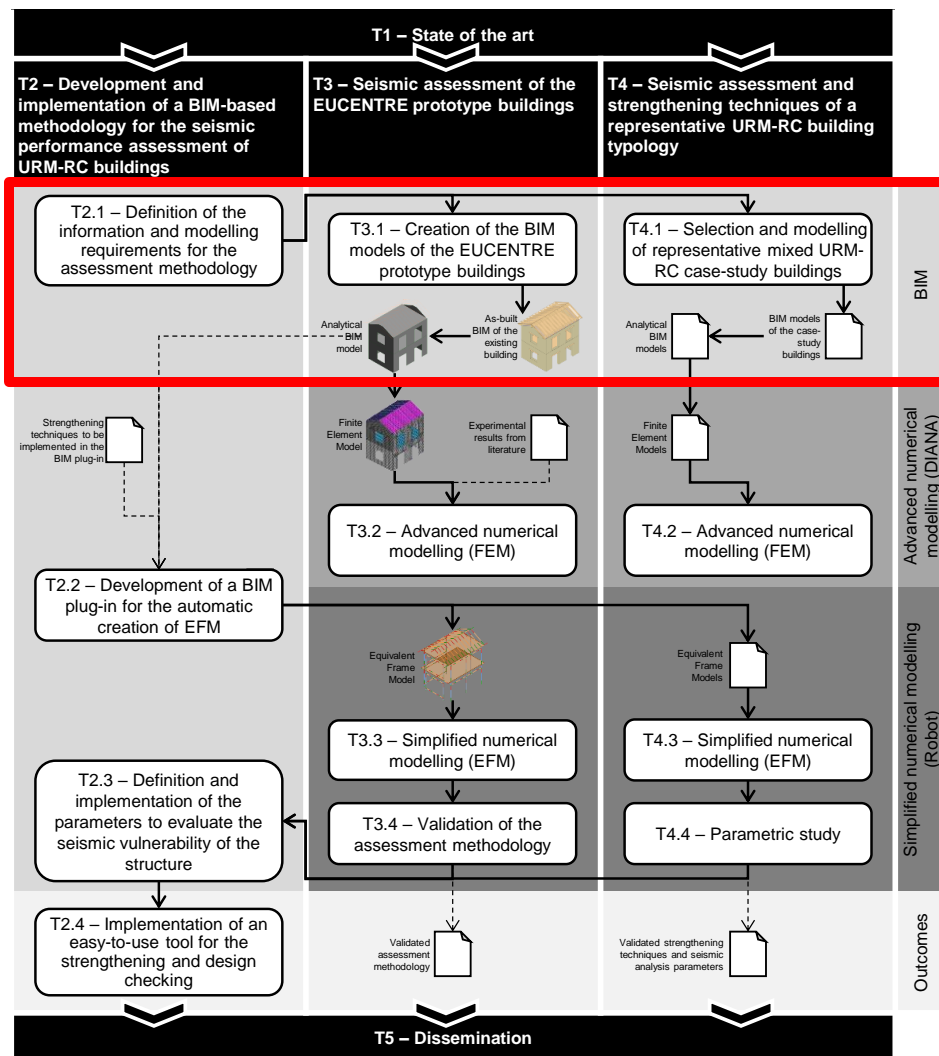
 **Future work** — Upcoming tasks

- **Thesis timeline and publications**

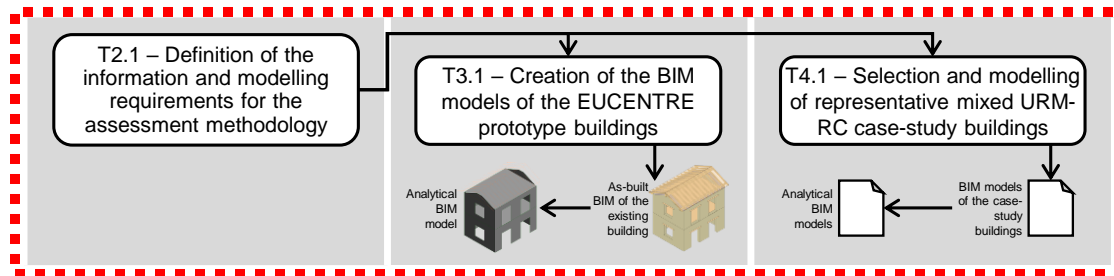
Tasks' flowchart



Creation of the BIM models



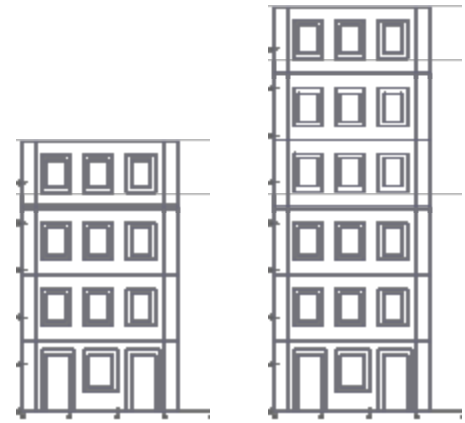
Creation of the BIM models



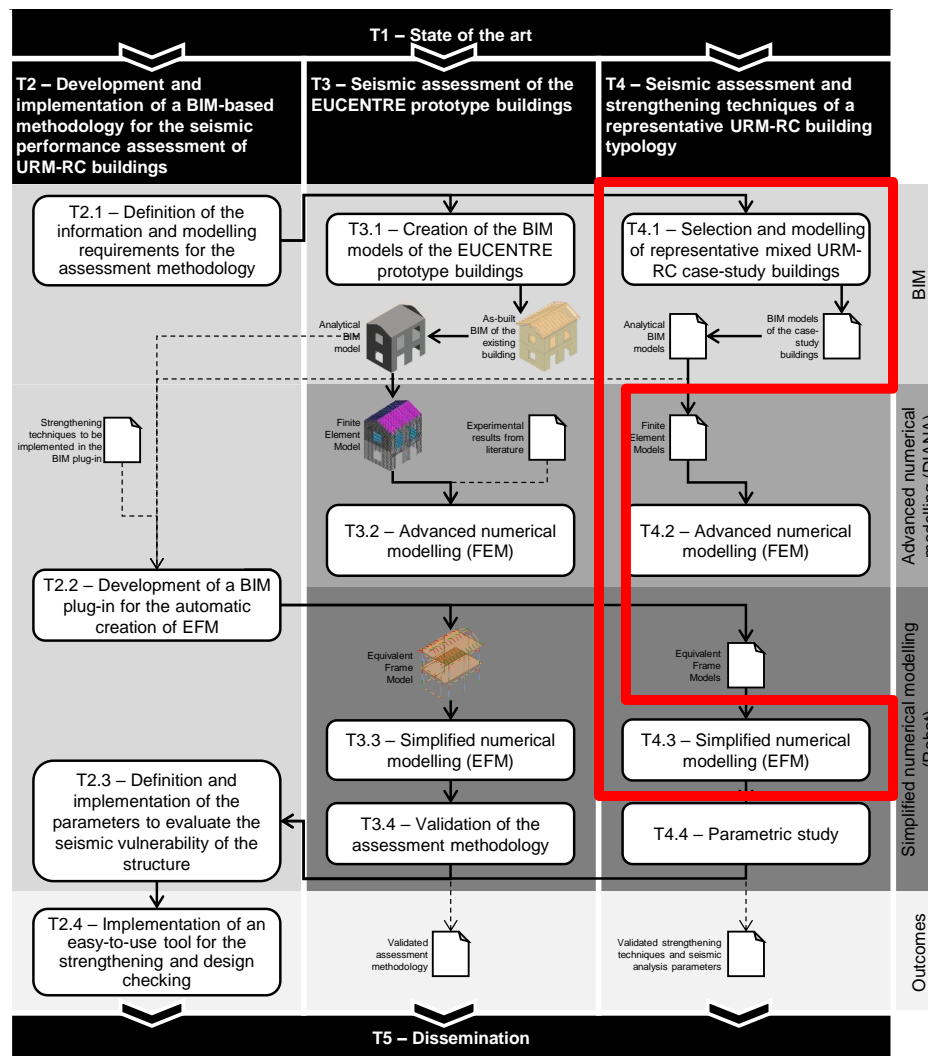
- ✓ Which building elements should be modelled (and how they should be modelled)
- ✓ Required level of detail (LOD)
- ✓ Required non-geometric attributes (material properties, boundary conditions, loads)

- ✓ EUCENTRE prototype buildings 1 and 3
- ✓ Software: Revit 2019
- ✓ BIM models are automatically converted to analytical 3D models (and exported to the structural analysis software)

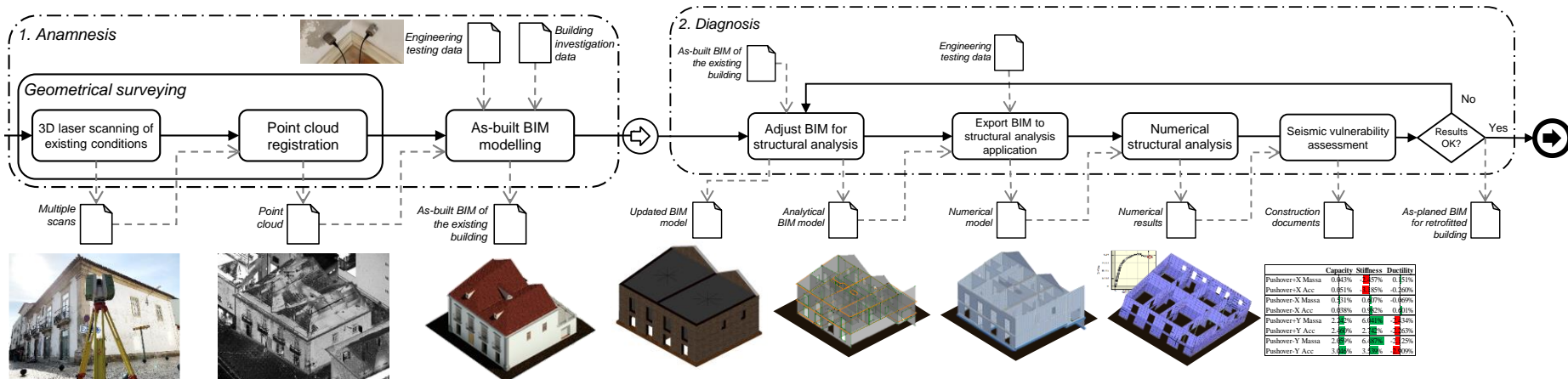
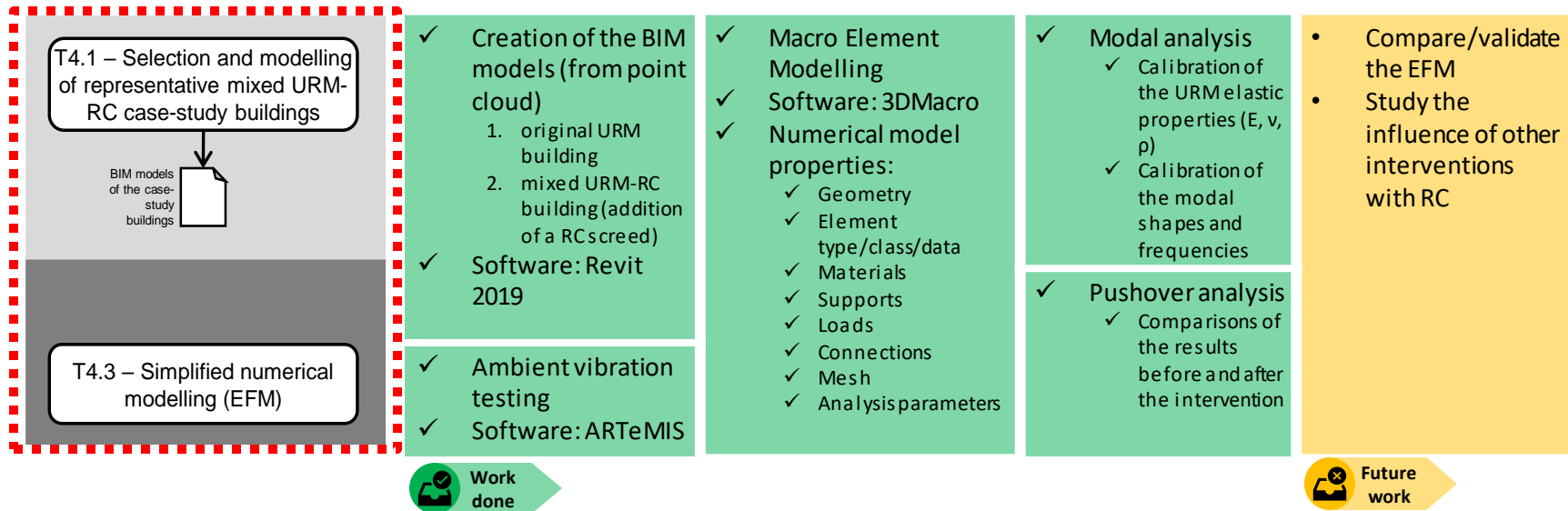
- Geometry, number of floors, openings, etc.
- Intervention typologies:
 - the **addition** of RC renders and/or jacketing;
 - the **insertion** of RC ring-beams at the top of external façade walls;
 - the **substitution** of timber floor diaphragms by RC slabs



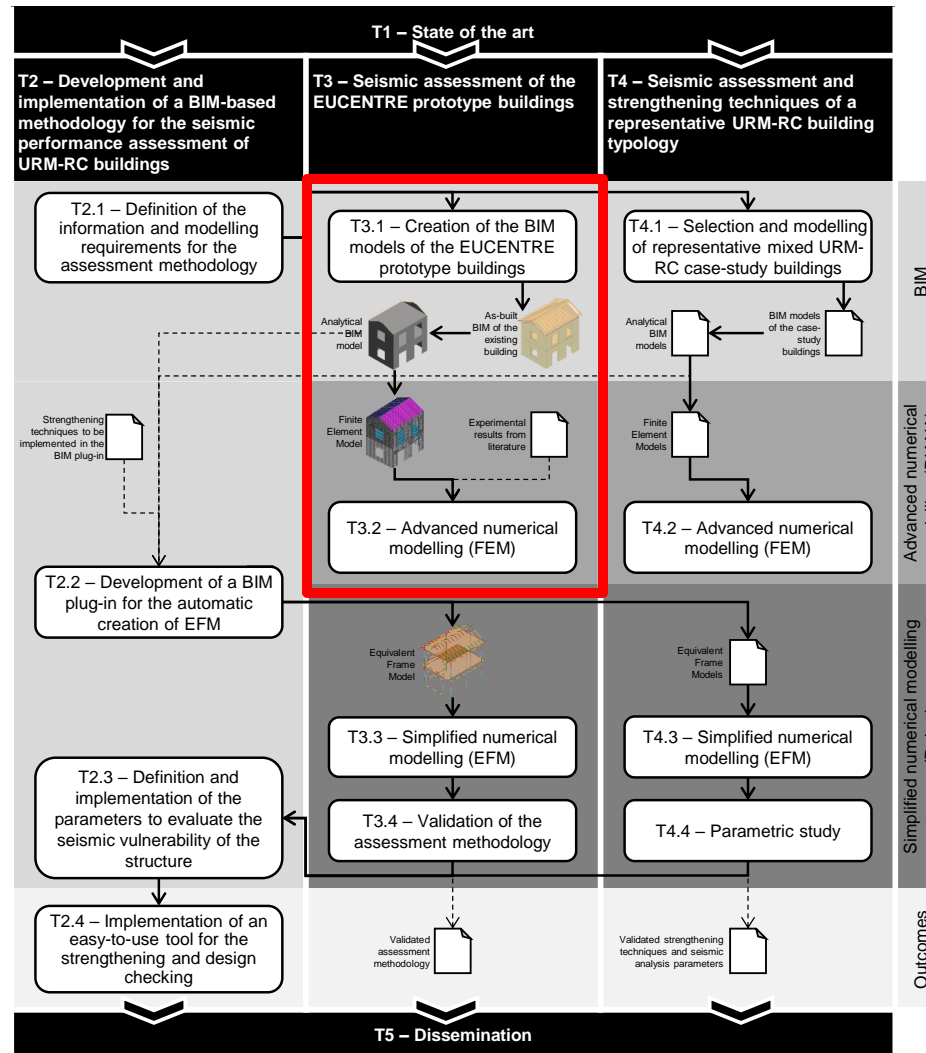
Intervention nature/type	A. Additions						
	Reinforced render or jacketing	Cooperating slabs (diaphragms)	New (shear) walls	Supplemental frames, beams or columns	Intermediate floors	Plan enlargement	Additional floors (raising)
B. Strengthening							
	Ring beams	Embedded frames	Seismic joints	Staircase	Corers	Underground structure	
C. Rehabilitation	Roof structure	Floor slab	Floor slabs	Walls (in the original position)	Reengineered frames	Whole floor refurbishment	Built-in structure ('facade')



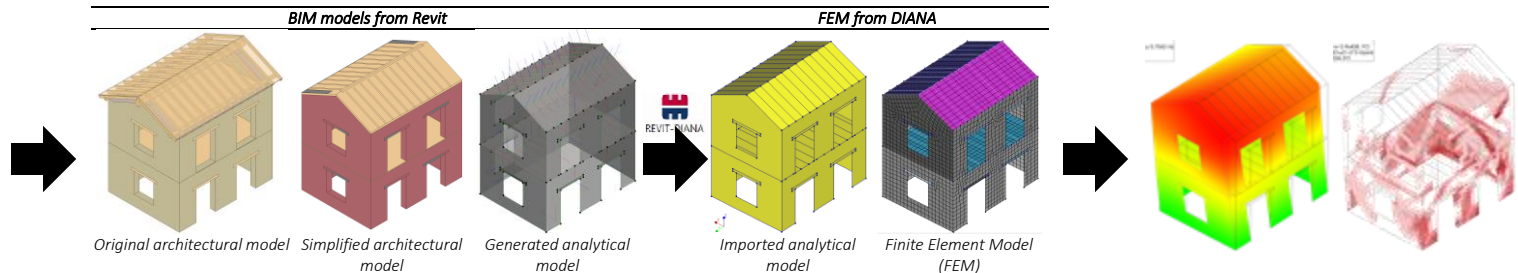
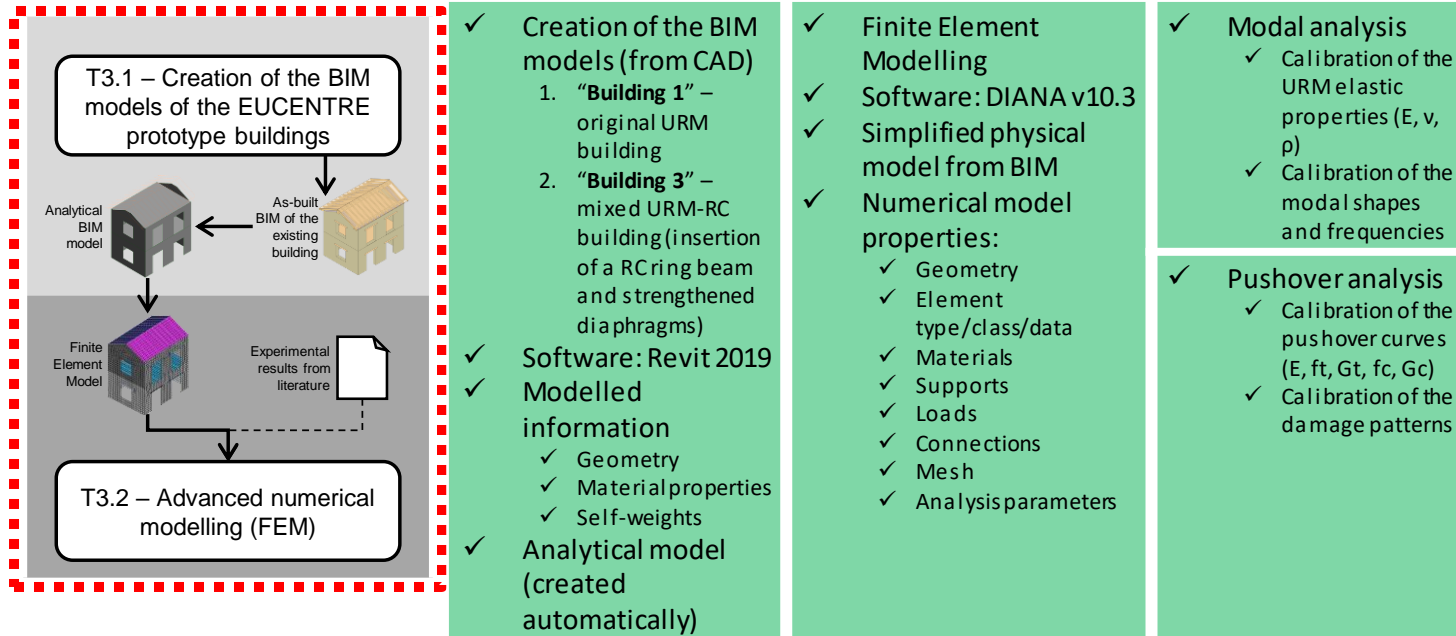
Case study I – Seismic performance assessment of an existing URM-RC building



**Case study II –
Validation based on
EUCENTRE
experimental results**



Case study II – Validation based on experimental results



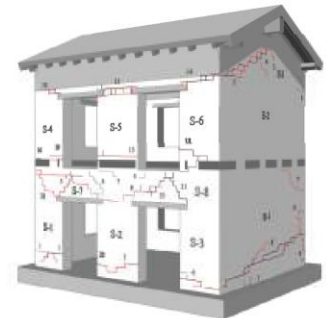
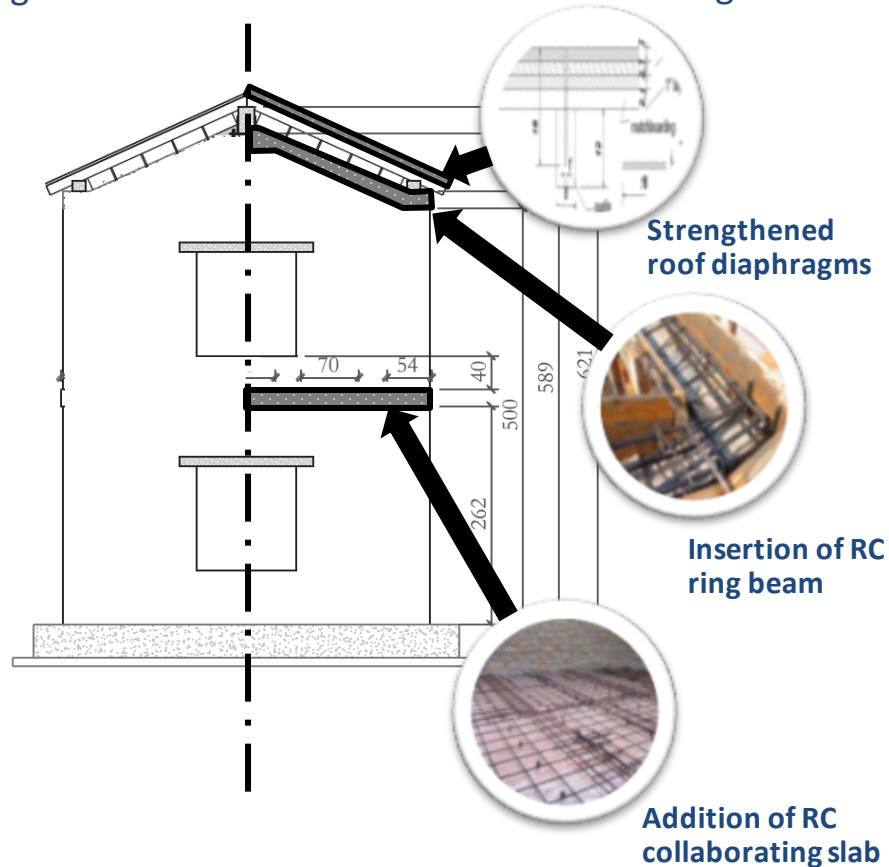
Case study II – Validation based on experimental results

“Building 1” – original URM building



Experimental setup (shaking table tests)

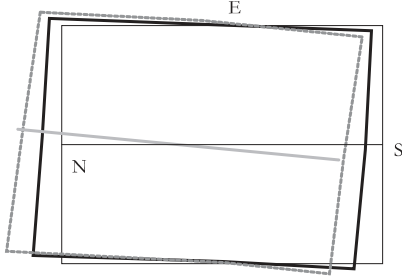
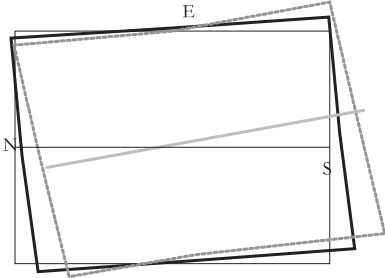
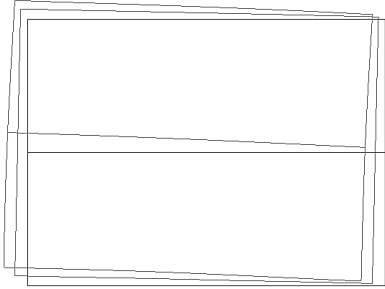

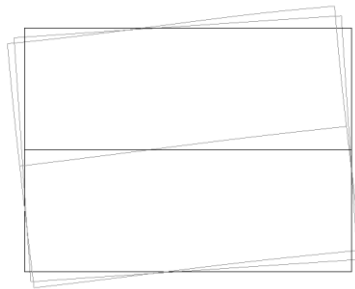
“Building 3” – mixed URM-RC building



Initial damage before experimental tests

Case study II – Calibration based on experimental results

Modal analysis

	Mode 1	Mode 2	Mode 3
Experimental analysis (dynamic test at 0.05 g) (Senaldi et al. 2014)	 <p>$f = 7.35 \text{ Hz}$</p>	Not available	 <p>$f = 14.05 \text{ Hz}$</p>
Numerical eigenvalue analysis (DIANA)	 <p>$f = 7.41 \text{ Hz}$ $\Delta f[\%] = 0.82\%$</p>	 <p>$f = 7.64 \text{ Hz}$</p>	 <p>$f = 12.10 \text{ Hz}$ $\Delta f[\%] = -13.88\%$</p>

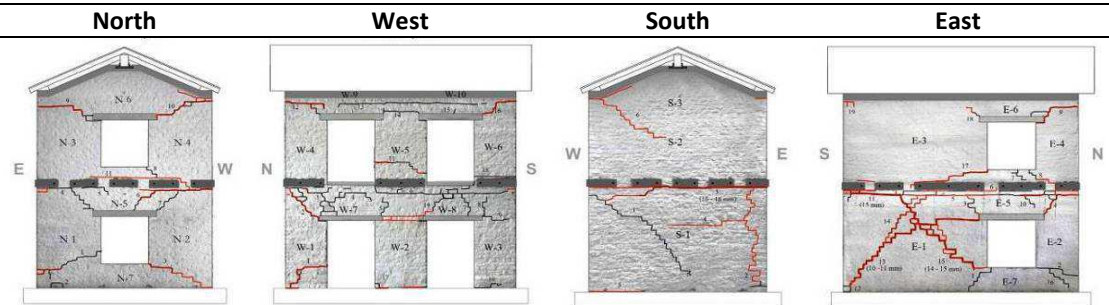
$E = 923 \text{ MPa}$

Case study II – Calibration based on experimental results

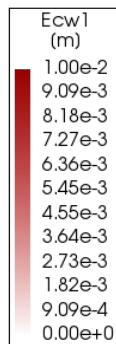
Damage patterns

Cracks induced after transportation to the shaking table (in black).

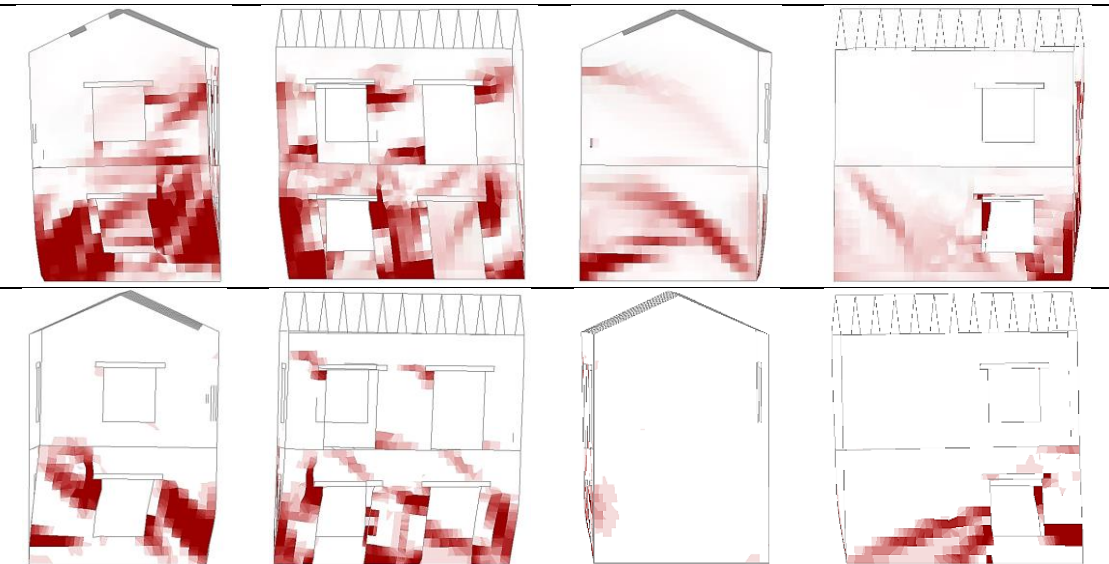
Cracks induced after the experimental test at nominal PGA of 0.6 g (in red) (Magenes and Penna 2011; Magenes et al. 2012).



Crack-widths obtained from DIANA (E_{cr1}, max of 5 layers) – Positive Y direction.



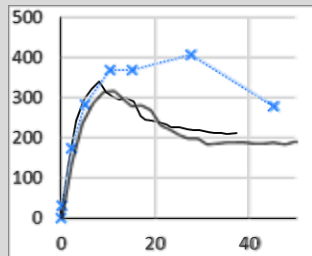
Crack-widths obtained from DIANA (E_{cr1}, max of 5 layers) – Negative Y direction.



Case study II – Calibration based on experimental results

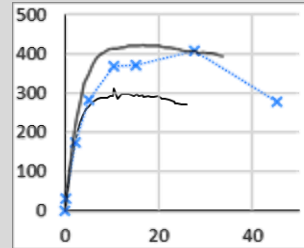
Influence of material properties

$E = 700000 \text{ kN/m}^2$
 500000 kN/m^2
 $f_t = 180 \text{ kN/m}^2$
 $G_t = 0.05 \text{ kN/m}$
 $f_c = 1000 \text{ kN/m}^2$
 $G_c = 1 \text{ kN/m}$



Influence of the load distribution and analysis parameters

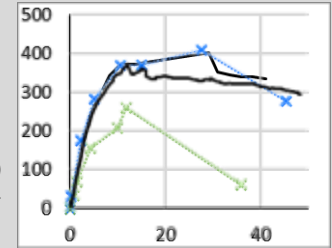
$E = 700000 \text{ kN/m}^2$
 $f_t = 138 \text{ kN/m}^2$
 $G_t = 0.35 \text{ kN/m}$
 $f_c = 700 \text{ kN/m}^2$
 $G_c = 6 \text{ kN/m}$
"PUSHOV", "Y"
"PUSHOV", "ALLDIR"



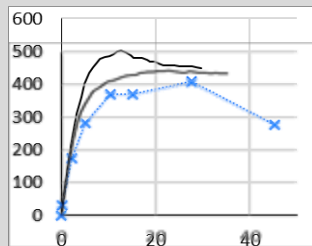
$E = 700000 \text{ kN/m}^2$
 $f_t = 138 \text{ kN/m}^2$
 $G_t = 0.35 \text{ kN/m}$
 $f_c = 700 \text{ kN/m}^2$
 $G_c = 6 \text{ kN/m}$

Time steps: 0.1(10) 0.5(5) 2(5)
 Conv. tolerance: 0.01

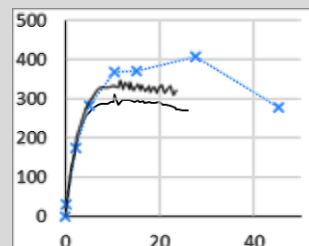
0.1(15) 0.2(5) 0.3(5) 0.4(5) 0.5(10)
 0.001



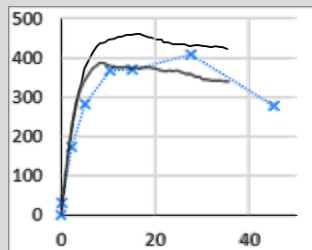
$E = 700000 \text{ kN/m}^2$
 $f_t = 200 \text{ kN/m}^2$
 100 kN/m^2
 $G_t = 0.35 \text{ kN/m}$
 $f_c = 1000 \text{ kN/m}^2$
 $G_c = 6 \text{ kN/m}$



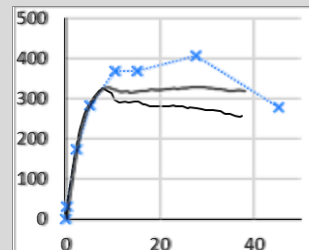
$E = 700000 \text{ kN/m}^2$
 $f_t = 138 \text{ kN/m}^2$
 $G_t = 0.35 \text{ kN/m}$
 $f_c = 2000 \text{ kN/m}^2$
 700 kN/m^2
 $G_c = 6 \text{ kN/m}$



$E = 700000 \text{ kN/m}^2$
 $f_t = 138 \text{ kN/m}^2$
 $G_t = 0.35 \text{ kN/m}$
 0.1 kN/m
 $f_c = 1000 \text{ kN/m}^2$
 $G_c = 6 \text{ kN/m}$

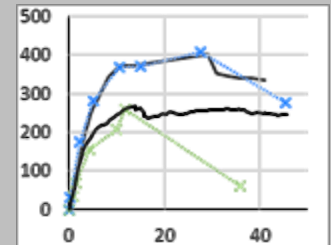


$E = 700000 \text{ kN/m}^2$
 $f_t = 100 \text{ kN/m}^2$
 $G_t = 0.05 \text{ kN/m}$
 $f_c = 1000 \text{ kN/m}^2$
 $G_c = 4 \text{ kN/m}$
 1 kN/m



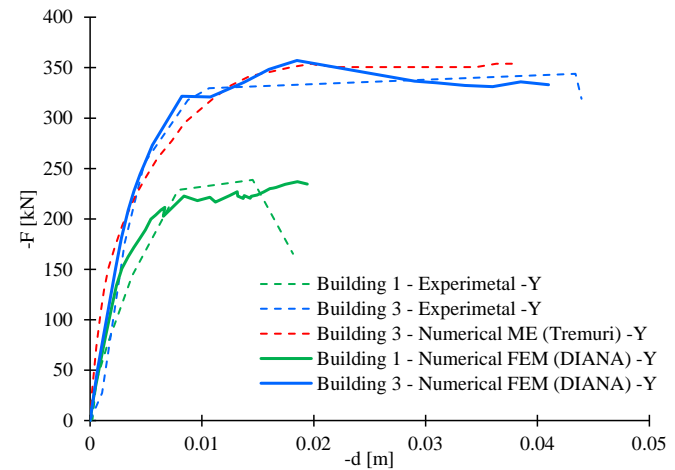
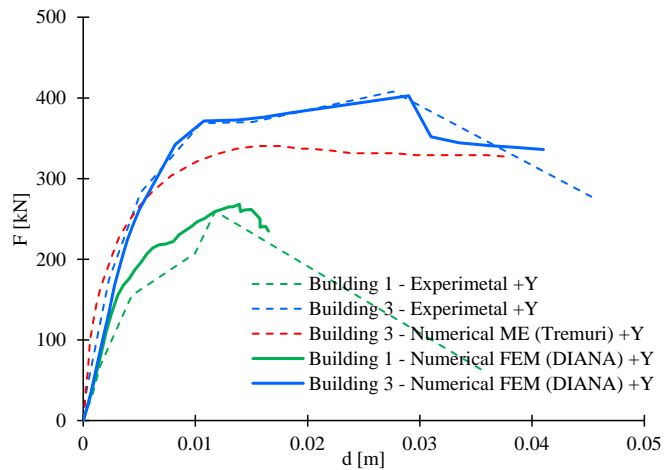
Influence of the building typology

$E = 500000 \text{ kN/m}^2$
 $f_t = 180 \text{ kN/m}^2$
 $G_t = 0.05 \text{ kN/m}$
 $f_c = 1000 \text{ kN/m}^2$
 $G_c = 6 \text{ kN/m}$
Mixed URM-RC
Original URM



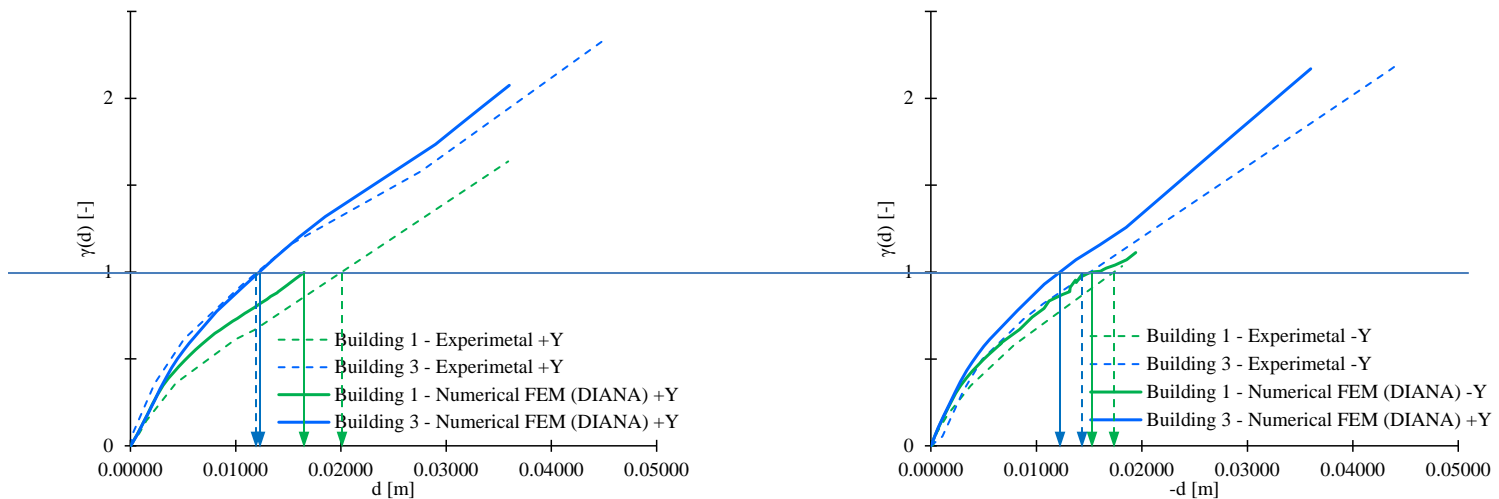
Case study II – Pushover results

Pushover curves



Case study II – Pushover results

Target displacement of the SDoF system *versus* the percentage of the seismic action ($\gamma(d)$)



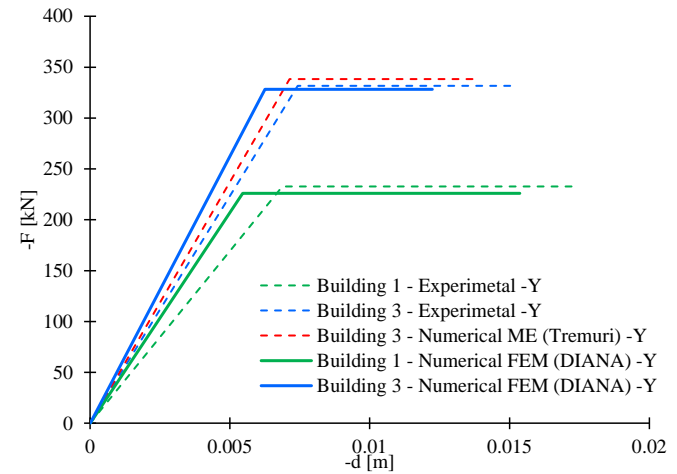
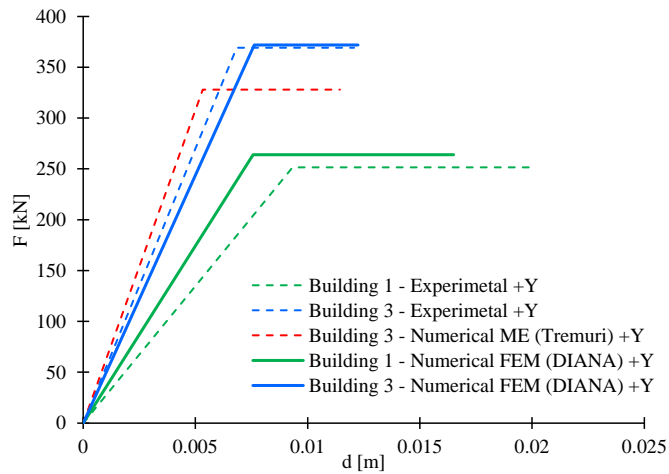
Scale factor for the initial seismic demand, $\gamma(d)$

$$T^*(d^*) < T_C \quad \gamma(d^*) = \frac{S_a(d^*) \cdot T^*(d^*) \cdot T_C - S_a(d^*) \cdot (T^*(d^*))^2 + d^* \cdot 4\pi^2}{S_{ae}(d^*) \cdot T^*(d^*) \cdot T_C}$$

$$T^*(d^*) \geq T_C \quad \gamma(d^*) = \frac{d^* \cdot 4\pi^2}{S_{ae}(d^*) \cdot (T^*(d^*))^2}$$

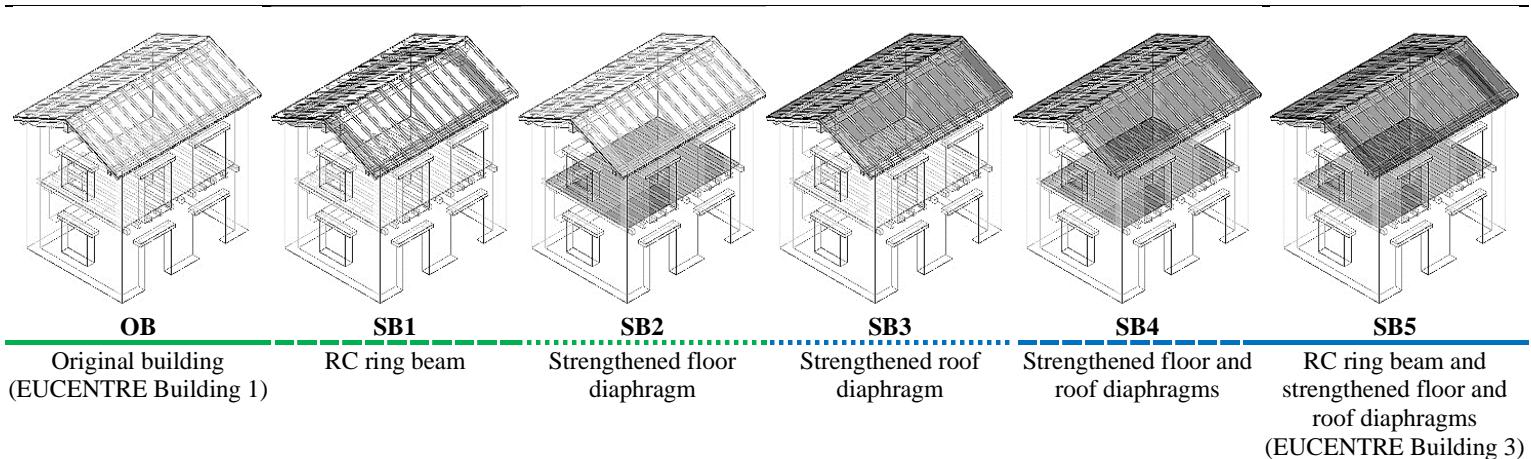
Case study II – Pushover results

Idealised elasto-perfectly plastic force displacement relationships (N2 method)



Case study II – Pushover results

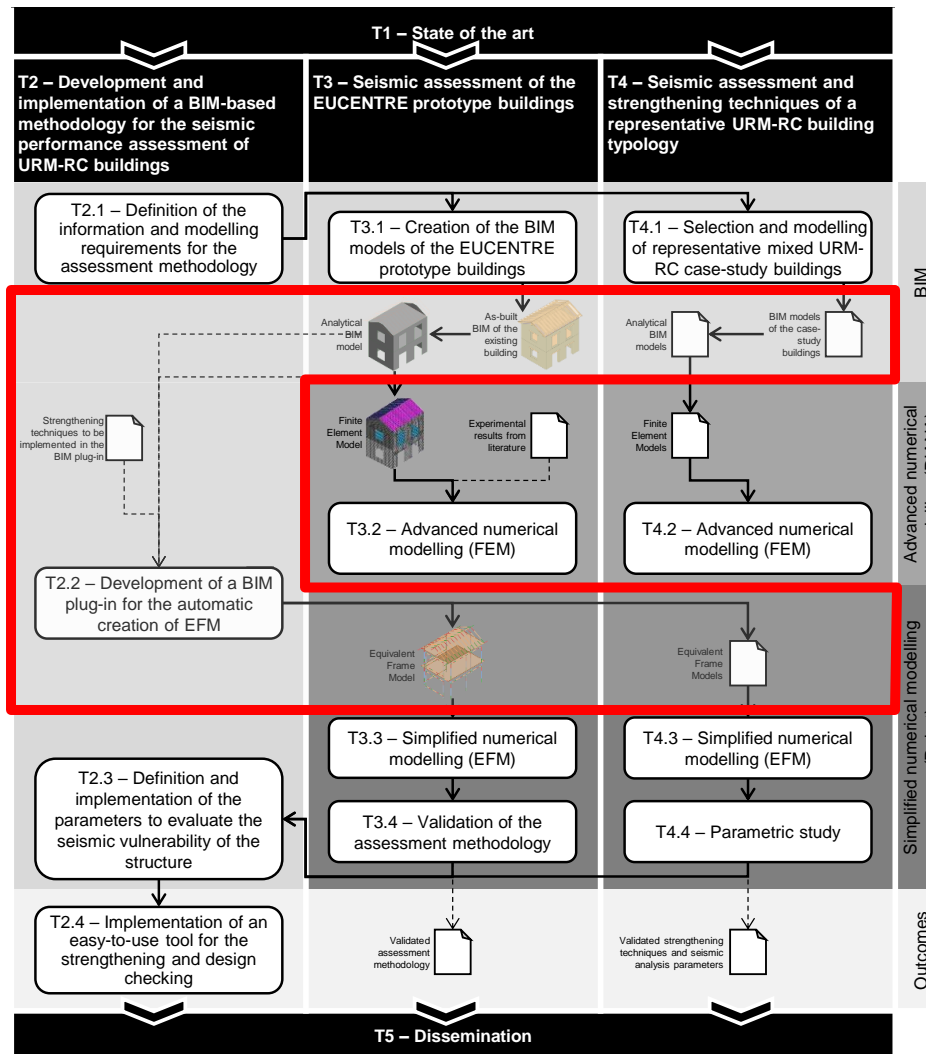
Comparison of the results obtained from the models with and without the strengthening elements



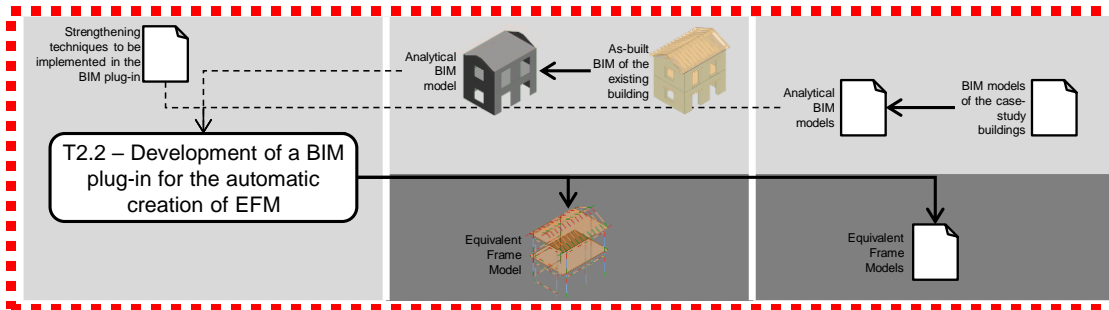
		Capacity (Fy)	Stiffness (Fy/dy)	Ductility ratio (du/dy)
(+Y)	Numerical (DIANA)	(SB1)/(OB)-1	18.5%	123.8%
		(SB2)/(OB)-1	32.5%	118.8%
		(SB3)/(OB)-1	16.8%	132.6%
		(SB4)/(OB)-1	43.9%	107.3%
	Numerical (DIANA)	(SB5)/(OB)-1	43.6%	144.4%
	Experimental	(SB5)/(OB)-1	46.8%	203.9%
(-Y)	Numerical (DIANA)	(SB1)/(OB)-1	40.9%	98.3%
		(SB2)/(OB)-1	45.4%	241.7%
		(SB3)/(OB)-1	27.9%	313.4%
		(SB4)/(OB)-1	52.4%	245.9%
	Numerical (DIANA)	(SB5)/(OB)-1	51.8%	321.1%
	Experimental	(SB5)/(OB)-1	42.5%	160.1%

$$\Delta\% = \left[\frac{\text{Strengthened Building}}{\text{Original Building}} - 1 \right] \times 100$$

**Creation of
the
Equivalent
Frame
Models**



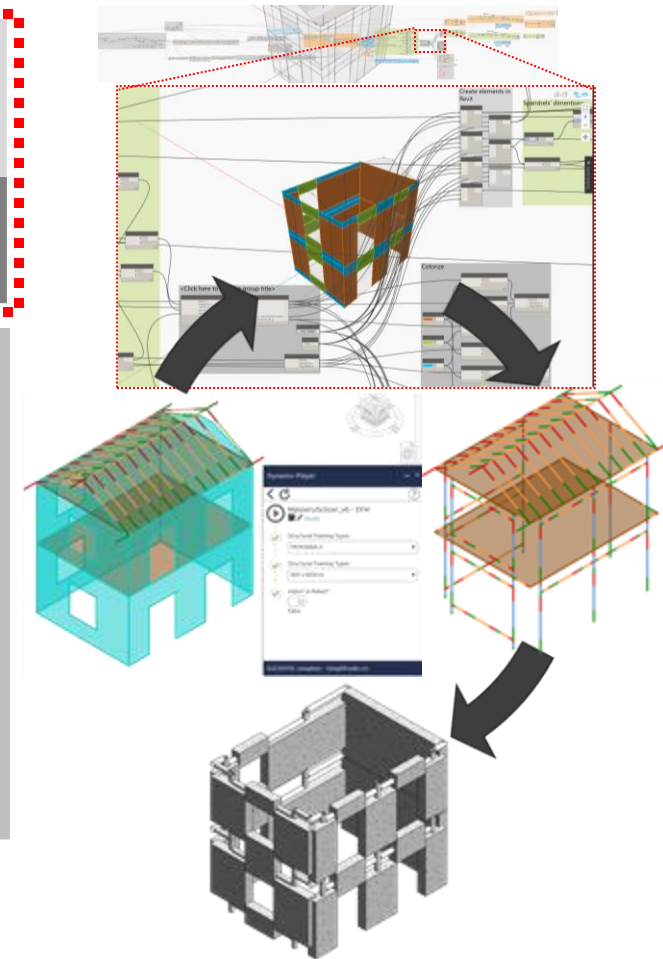
Creation of the Equivalent Frame Models

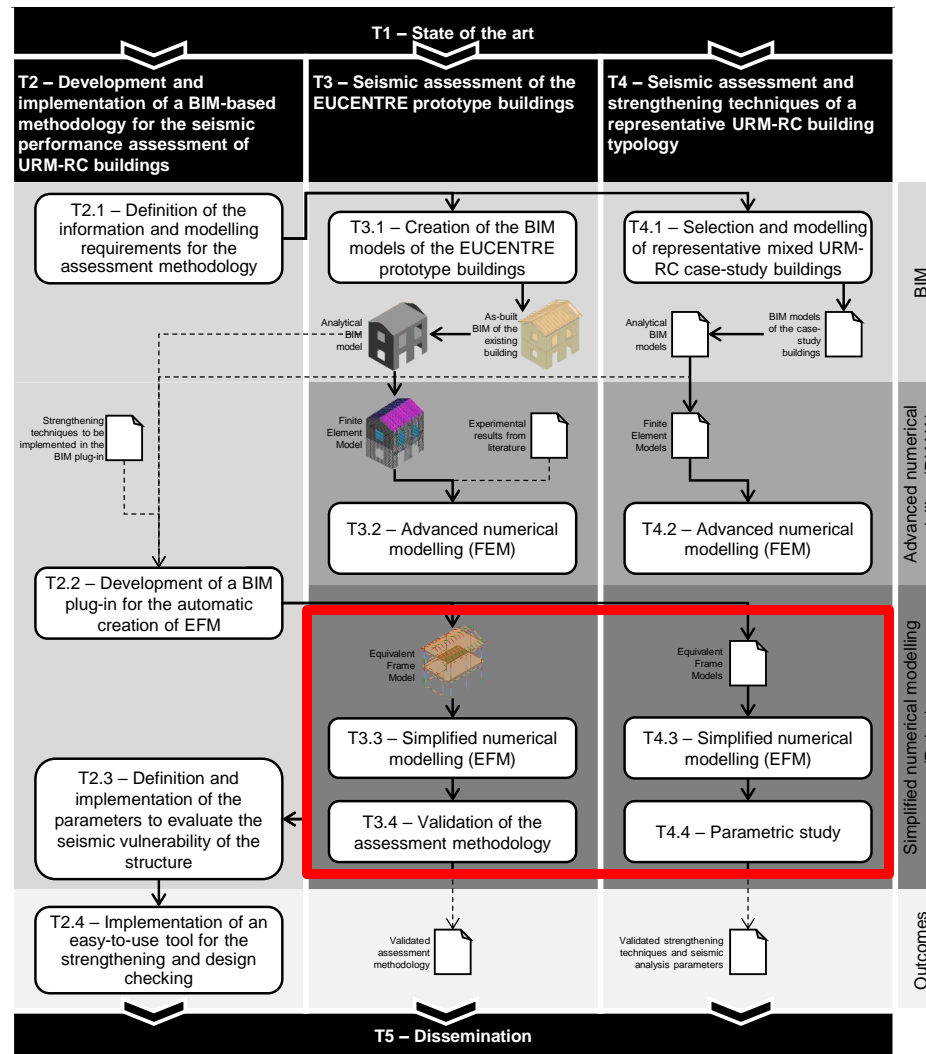


- ✓ Revit plug-in based on a python script written in the Revit API
- ✓ Implemented workflow
 1. Selection of elements
 2. Wall discretization (piers, spandrels, rigid nodes)
 3. Element identification
 4. EF idealization
 5. Properties assignment
 6. Export to the analysis software

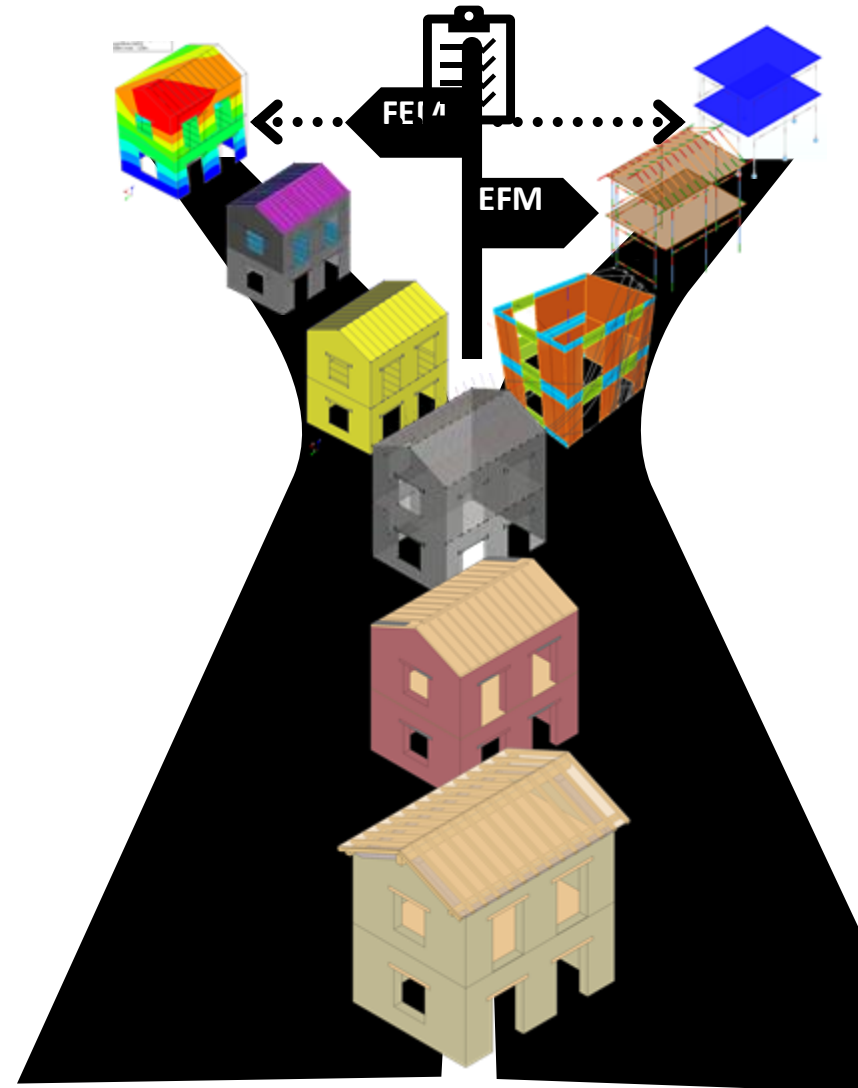
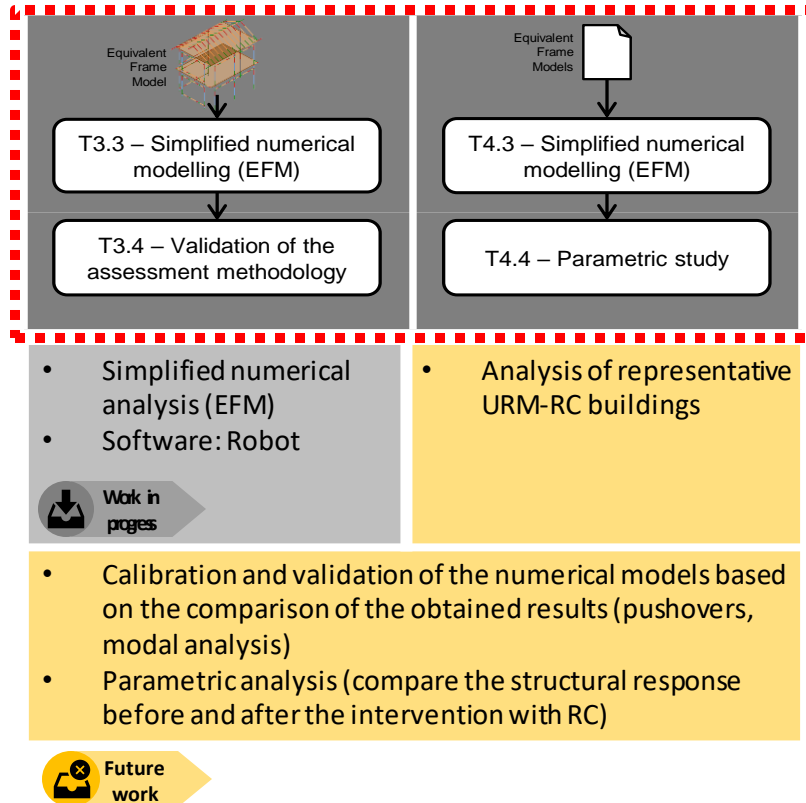
- ✓ Input: Analytical BIM models
- ✓ Output: EFM

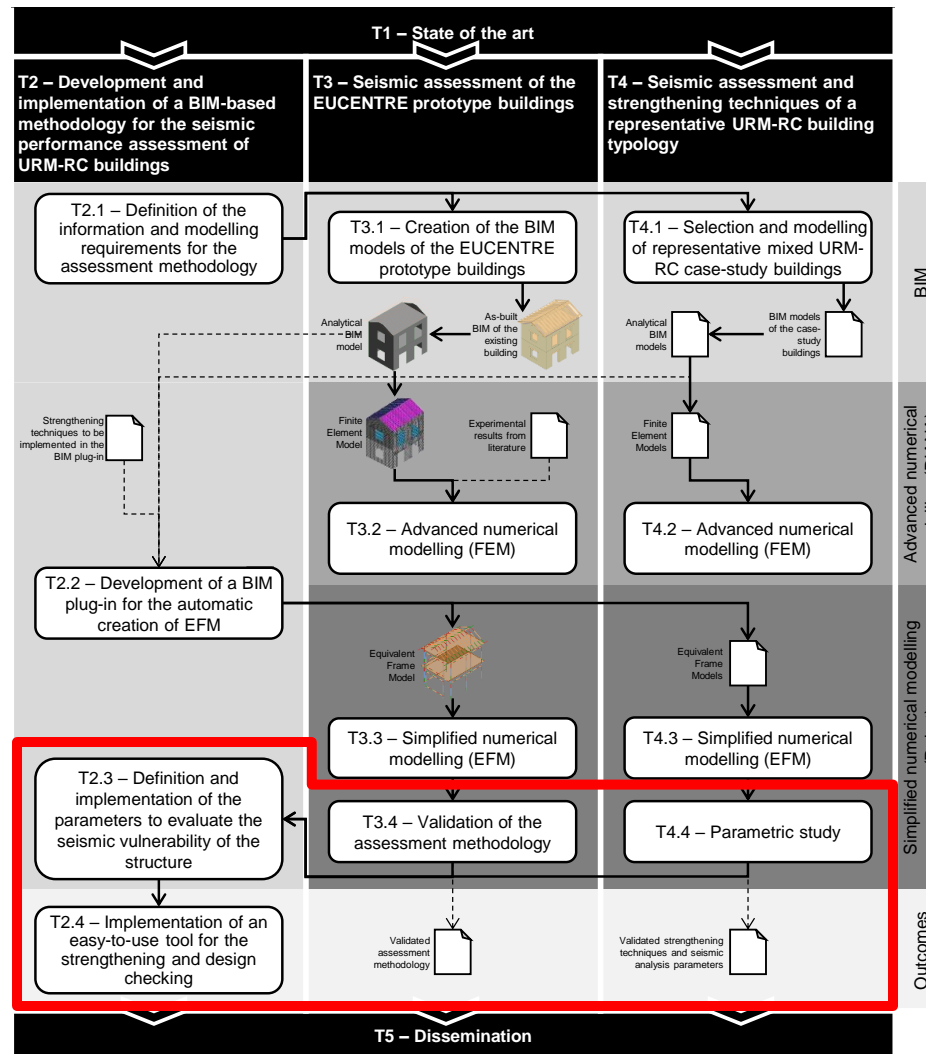
- Input: Analytical BIM models (and material properties)
- Output: EFM



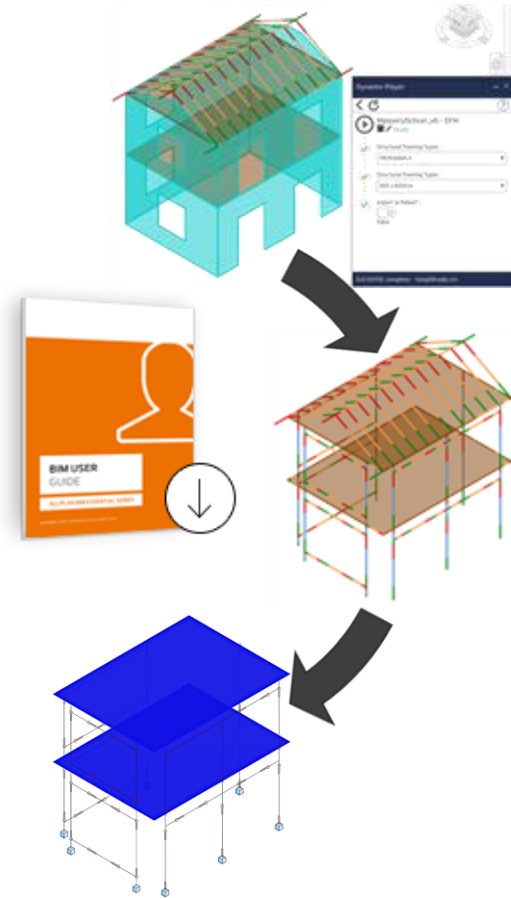
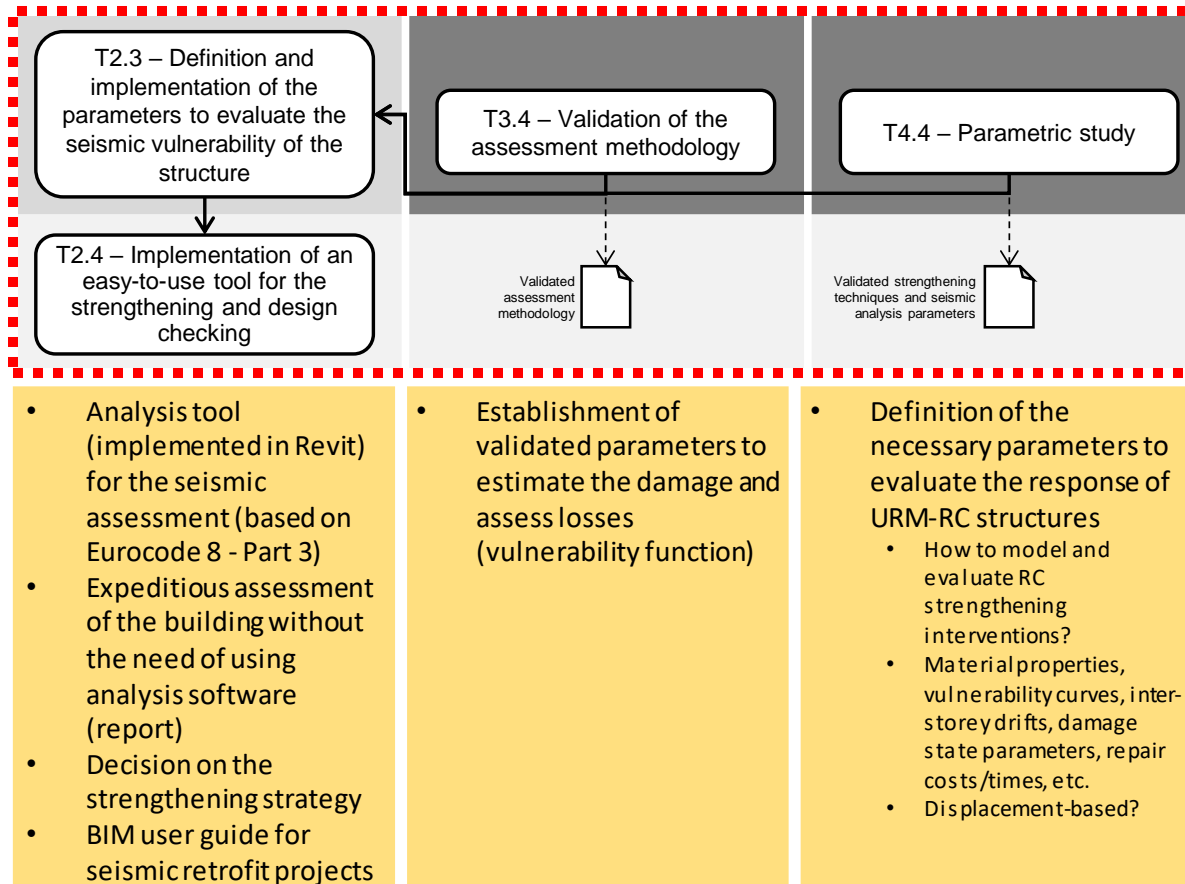


Analysis of the EFM and validation based on numerical results

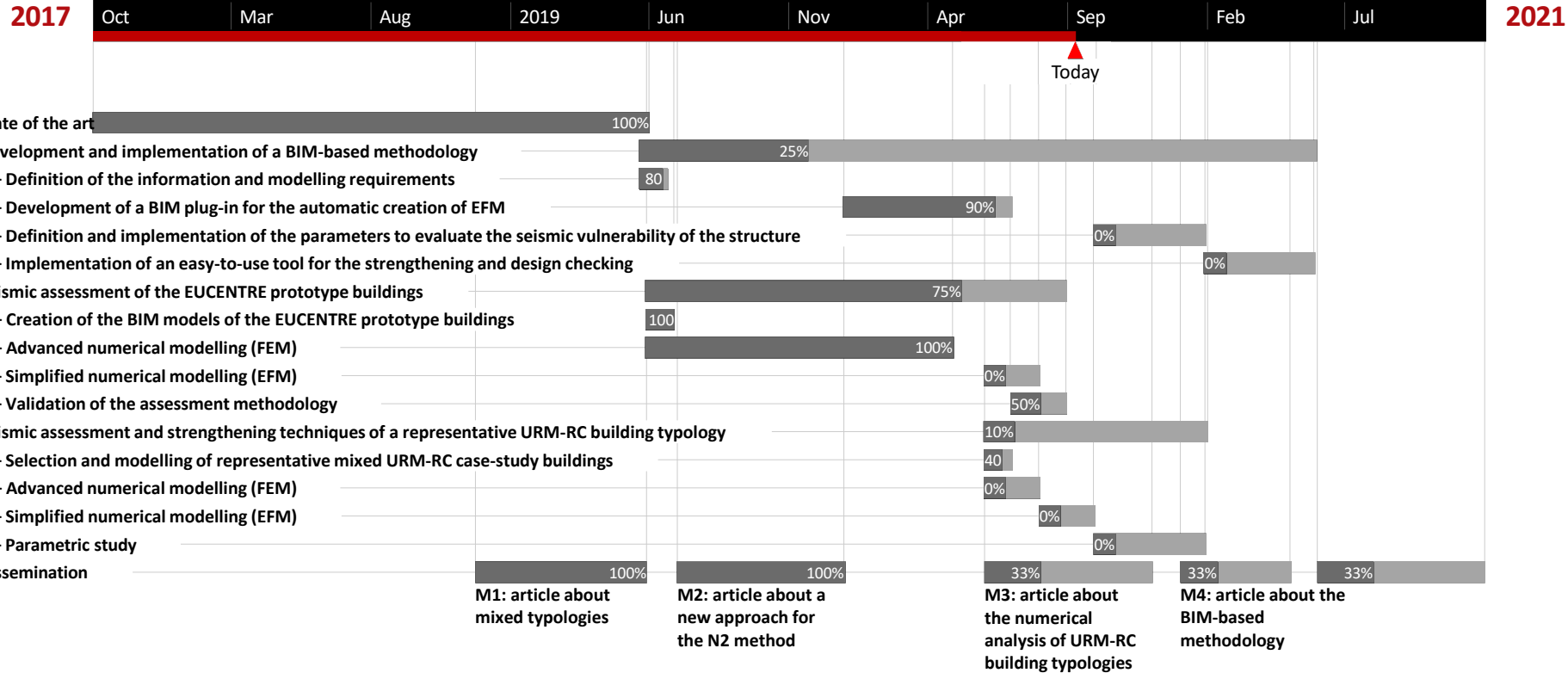




Development and implementation of the assessment methodology



Thesis timeline



Current impact

- Articles in International Journals

Published



Intervened URM buildings with RC elements: typological characterisation and associated challenges

Lopes, G. C., Vicente, R., Ferreira, T. M., & Azenha, M. (2019).

Bulletin of Earthquake Engineering, 1-33.



Displacement-based seismic performance evaluation and vulnerability assessment of buildings: The N2 method revisited

Lopes, G. C., Vicente, R., Ferreira, T. M., Azenha, M., & Estêvão, J. (2020).

Structures (24), 41-49.

Submitted



Numerical simulations of derived URM-RC buildings: assessment of strengthening interventions with RC

Lopes, G. C., Mendes, N., Vicente, R., Ferreira, T. M., & Azenha, M. (2020).

(Journal of Building Engineering?)

- Conference articles



BIM-based methodology for the seismic performance assessment of existing buildings

Lopes, G. C., Vicente, R., Ferreira, T. M., Azenha, M., & Rodrigues, H. (2020).

ENCORE 2020.



Desafios e direções de investigação na identificação e caracterização de tipologias de edifícios de alvenaria intervencionados com recurso a betão armado

Lopes, G. C., Vicente, R., Ferreira, T., & M., Azenha, M. (2019).

SÍSMICA 2020.

- Articles in National Journals



BIM-based methodology for the seismic performance assessment of existing buildings

Lopes, G. C., Vicente, R., Ferreira, T. M., Azenha, M., & Rodrigues, H. (2020).

Revista portuguesa de engenharia de estruturas 2020.

Thank you for your attention!

Gonalo Correia Lopes

PhD candidate in Civil Engineering

email: gclopes@ua.pt

Thesis title: **A BIM-based methodology for the seismic performance assessment of existing URM-RC buildings**

Acknowledgements are due to the PhD grant PD/BD/135201/2017 provided by Foundation for Science and Technology (FCT) within the scope of the Doctoral Programme InfraRisk- (Analysis and Mitigation of Risks in Infrastructures) and to University of Aveiro, FCT/MEC for the financial support to the research Unit RISCO – Aveiro Research Centre of Risks and Sustainability in Construction – (FCT/UID/ECI/04450/2013)