# Analysis of RC buildings under earthquakes with arbitrary orientations.

## **Results and Challenges**

PhD student: Despoina Skoulidou, FEUP Scientific advisor: Xavier Romão, FEUP



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universidade de aveiro

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ANALYSIS AND MITIGATION OF RISKS IN INFRASTRUCTURES | INFRARISK-Porto, Portugal, July 8 2016 The angle of seismic incidence in the seismic safety assessment procedure of individual buildings

Eurocode 8 Part 3 4stage procedure: (deterministically-oriented approach) 1) Limit State/s 2) Level of knowledge 3) Structural analysis 4) Safety verifications PBEE framework (Probabilistic approach)  $\lambda(L) = \iint G(L \mid DM) \cdot dG(DM \mid EDP) \cdot dG(EDP \mid IM) \cdot dP(IM)$ Decision!

The angle of seismic incidence in the seismic safety assessment procedure of individual buildings



The angle of seismic incidence in the seismic safety assessment procedure of individual buildings



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- Practical
- ✓ EDP
- Frequency content
  - ✓ Seismic intensity
    - ✓ Behaviour factor

Inexistent techniques to predict the critical angle.

Analytical procedure proposed for LFA.

Conceptual 
 Overall performance of a 
 realistic 3D structure and 
 compliance (or not) with 
 a Limit State.
 Unique demand parameter 
 able to characterize the 
 global response of the 
 structure:

Practical

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Combination of the two orthogonal components using a directional combination rule,

 $F(\alpha) = \begin{cases} m \cdot 2.5 \cdot a_g \cdot S \cdot \eta \cdot \frac{T_C}{T(\alpha)} &, \text{ for } 0 \le \alpha \le \alpha_{T_C} \\ m \cdot 2.5 \cdot a_g \cdot S \cdot \eta &, \text{ for } \pi \cdot \alpha_{T_C} \le \alpha \le \alpha_{T_C} \\ m \cdot 2.5 \cdot a_g \cdot S \cdot \eta \cdot \frac{T_C}{T(\alpha)} &, \text{ for } \pi - \alpha_{T_C} \le \alpha \le \pi + \alpha_{T_C} \\ \dots \end{cases}$ 

e.g. a percentage  $\lambda$  combination rule:

$$\mathbf{u}^{A}(\alpha) = \sqrt{\left(F(\alpha) \cdot \mathbf{u}_{\mathrm{I},"1"}^{A}(\alpha) \pm \lambda \cdot F(\alpha + \frac{\pi}{2}) \cdot \mathbf{u}_{\mathrm{I},"1"}^{A}(\alpha + \frac{\pi}{2})\right)^{2} + \left(F(\alpha) \cdot \mathbf{u}_{\mathrm{II},"1"}^{A}(\alpha) \pm \lambda \times F(\alpha + \frac{\pi}{2}) \cdot \mathbf{u}_{\mathrm{II},"1"}^{A}(\alpha + \frac{\pi}{2})\right)^{2}}$$
  
or the SRSS:

$$\mathbf{u}^{A}(\alpha) = \sqrt{\left(\sqrt{\left[F(\alpha) \cdot \mathbf{u}_{I,"1"}^{A}(\alpha)\right]^{2} + \left[F(\alpha + \frac{\pi}{2}) \cdot \mathbf{u}_{I,"1"}^{A}(\alpha + \frac{\pi}{2})\right]^{2}}\right)^{2} + \left(\sqrt{\left[F(\alpha) \cdot \mathbf{u}_{II,"1"}^{A}(\alpha)\right]^{2} + \left[F(\alpha + \frac{\pi}{2}) \cdot \mathbf{u}_{II,"1"}^{A}(\alpha + \frac{\pi}{2})\right]^{2}}\right)^{2}}$$



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Maximize to get the critical angle:
$$\frac{\mathrm{d}\mathbf{u}^{\mathbf{A}}(\alpha)}{\mathrm{d}\alpha} = 0 \quad \rightarrow \quad \alpha_{\mathrm{crit}}$$

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Analytical procedure proposed for LFA.

Conceptual 

 Overall performance of a realistic 3D structure and compliance (or not) with a Limit State.

 Unique demand parameter able to characterize the global response of the structure:

#### Global structural 3D response: Preliminary results

- Definition of one demand parameter able to describe the average global response: <u>Initial approach</u>
  - ✓ Proposed parameter: drift of the Centre of Mass,  $dr_{CM}$
  - ✓ Global response: Average drift of all columns,  $dr_{ave}$
  - ✓ Hypothesis: Both response parameters attain their maximum value for the same angle of seismic incidence,  $\theta_{dr_{CM}=\max} = \theta_{dr_{ave}=\max}$



#### Global structural 3D response: Preliminary results

• Structures analyzed (plasticity lumped at member ends)



Structure

No

1

2

3

4

5

#### Global structural 3D response: Preliminary results



#### Global structural 3D response: revised approach

 Definition of one demand parameter able to describe the average global response: <u>revised approach being proposed</u>.

- Proposed parameter: the interstorey drift remains the main suspect for the global demand parameter.
- ✓ Global demand: in terms of structural losses.
- ✓ Hypothesis: Definition of a point where the structural loss, quantified based on its drift, is correlated to the total structural loss.

How:

- Determination of structural loss of a storey using an element-based approach based on chord rotation – loss functions (Haselton et al., 2008).
- Structural loss of a storey using empirical EDP loss functions (Ramirez & Miranda, 2009).

Seismic safety assessment of 3D structures integrating the critical angle

Practical

Procedures to determine the critical angle of incidence of a response parameter.

e.g. methodology proposed for LFA.

Conceptual —

Definition of a response parameter able to describe global structural performance.

e.g. interstorey drift expressing total structural loss Maximizing the global response parameter with respect to the angle of incidence in order to obtain the total critical structural response.